



# Quartz-enhanced photoacoustic NH<sub>3</sub> sensor exploiting a large-prong-spacing quartz tuning fork and an optical fiber amplifier for biomedical applications

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## ABSTRACT

A sensor system for exhaled ammonia (NH<sub>3</sub>) monitoring exploiting quartz-enhanced photoacoustic spectroscopy (QEPAS) was demonstrated. An erbium-doped fiber amplifier (EDFA) with an operating frequency band targeting an NH<sub>3</sub> absorption line falling at 1531.68 nm and capable to emit up to 3 W of optical power was employed. A custom T-shaped grooved QTF with prong spacing of 1 mm was designed and realized to allow a proper focusing of the high-power optical beam exiting the EDFA between the prongs. The performance of the realized sensor system was optimized in terms of spectrophone parameters, laser power and modulation current, resulting in a NH<sub>3</sub> minimum detectable concentration of 14 ppb at 1 s averaging time, corresponding to a normalized noise equivalent absorption coefficient (NNEA) of  $8.15 \times 10^{-9} \text{ cm}^{-1} \text{ W}/\sqrt{\text{Hz}}$ . Continuous measurements of the NH<sub>3</sub> level exhaled by 3 healthy volunteers was carried out to demonstrate the potentiality of the developed sensor for breath analysis applications.

## 1. Introduction

In the field of medical diagnostics, an increasing number of studies have demonstrated that pathological diagnosis based on respiratory analysis is non-invasive and reliable [1–3]. Abnormal elevated levels of metabolites in exhaled breath herald the deterioration of physical conditions. For instance, normally the amount of ammonia (NH<sub>3</sub>) exhaled from the alveoli is several hundred parts per billion in concentration, while a rising ammonia level (>1 ppm) exhaled from humans have been linked to kidney and liver failure [4,5]. Narasimhan et al. have confirmed that there is a strong correlation between the level of respiratory ammonia and blood urea nitrogen (BUN) in patients with end-stage renal disease during hemodialysis [6]. Therefore, real-time measurement of ammonia in exhaled breath is not only used as an indicator of renal failure, but also determines the progress of hemodialysis process.

In order to realize continuous and online ammonia monitoring in

exhaled breath, there are two main sensor requirements: (1) ppb-level detection sensitivity; (2) fast response time. Up to now, various technologies for detection of ammonia have been reported, such as carbon nanomaterials [7], chemiluminescence analysis [8], photocatalytic technology [9] and ion chromatography method [10]. However, the presence of interfering substance (molecular impurities, electrolytes and nitrogen oxide) can adversely affect the accuracy of these methods. Moreover, most of these methods have long response time and poor detection sensitivity. Laser-based spectroscopic methods have been widely demonstrated to provide high detection sensitivity and fast measurement time [11–14]. Cavity ring-down spectroscopy (CRDS) is a direct absorption spectroscopy technique, in which laser is injected into a high-precision optical cavity composed of ultra-high reflectivity mirror. The intensity of laser exiting the cavity decreases exponentially with time, and the corresponding cavity ring-down time depends on the target gas concentrations in the cavity. Compared with traditional absorption spectroscopy techniques, CRDS exhibits high sensitivity

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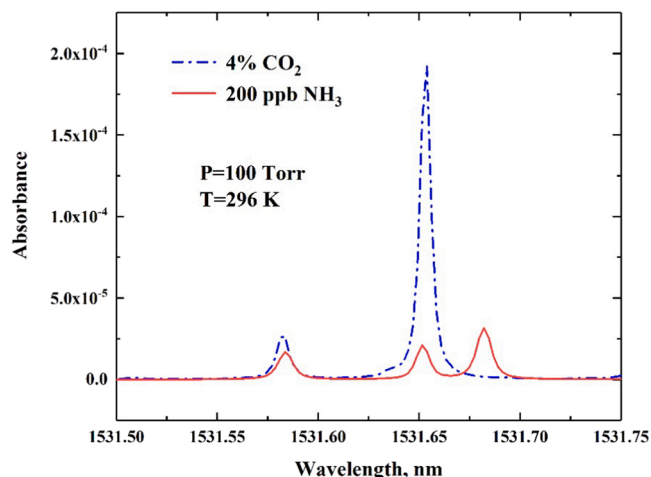


Fig. 1. Simulated absorbance of 200 ppb  $\text{NH}_3$  (solid line) and 4%  $\text{CO}_2$  (dash-dotted line) at a pressure of 100 Torr.

because it is not affected by variations in the incident laser intensity and benefits from long effective optical paths. For example, Manne et al. have implemented a similar technique to achieve a sensitivity of 50 parts per billion for ammonia detection [4]. However, the large volume of the optical cavity causes a long retention time for target gas, resulting in a degraded time resolution of 20 s, which is inappropriate for applications requiring continuous and real-time gas monitoring of exhaled breath.

Photoacoustic spectroscopy (PAS) is another well-established technique owing to its relatively simple, real-time and zero-background signal [15–17], in which the optoacoustic signal is detected by broadband microphones to retrieve the trace gas concentration levels. Quartz-enhanced photoacoustic spectroscopy (QEPAS), an improved version of traditional PAS, employs a small-size, high-Q-factor quartz tuning fork (QTF) instead of a conventional microphone as a resonant acoustic transducer. The key innovation of QEPAS is the use of the QTF with high resonance frequency (up to several kHz) and narrow frequency band (few Hz or less), which results in an improved immunity of the QEPAS system to ambient noise [18–49]. Moreover, QEPAS has a simple spectrophone design and is capable to analyze trace-gas samples of few  $\text{mm}^3$  in volume, providing a high detection sensitivity level and fast response time, and hence is very suitable for detecting exhaled gas in real time, as demonstrated in [35,36].

A remarkable feature of QEPAS is that its detection sensitivity is in direct proportion to the optical excitation power, which provides an approach to further improve QEPAS detection sensitivity by employing high-power lasers or optical fiber amplifiers [37,38]. Nowadays commercially available erbium-doped fiber amplifiers (EDFAs) with

sophisticated technology have three telecommunication bands, i.e., S band (1450–1550 nm), C band (1520–1570 nm) and L band (1565–1610 nm). The first combination of a QTF-based QEPAS sensor and an EDFA for  $\text{H}_2\text{S}$  detection has been reported [39]. However, due to the limitation of 300- $\mu\text{m}$  prong spacing of QTF and the degraded beam quality caused by the EDFA, a large background noise was introduced.

In this manuscript, a  $\text{NH}_3$  sensor system aiming at real-time respiration monitoring is demonstrated, in which a novel custom QTF with prong spacing of 1 mm and an EDFA in the wavelength range of 1531–1540 nm were employed. Benefiting from the high output power of the EDFA, the wide prong spacing of the custom QTF and the small size of the QEPAS cell, a ppb-level detection sensitivity and rapid response time were achieved. To demonstrate its effectiveness for breath analysis applications, the  $\text{NH}_3$  QEPAS sensor was tested by measuring the ammonia levels exhaled by three healthy individuals.

## 2. Selection of target absorption line

Due to the presence of the fingerprint spectrum of gas molecules, the QEPAS technology based on Beer Lambert's law enables excellent selectivity as well as real-time measurement. Ammonia has a complex infrared spectrum with four fundamental vibrational modes ( $\nu_1$ ,  $\nu_2$ ,  $\nu_3$ ,  $\nu_4$ ). According to the HITRAN database,  $\text{NH}_3$  two perpendicular bands ( $\nu_1 + \nu_3$ ,  $2\nu_2^2$ ) are dominant in the vicinity of 1.5  $\mu\text{m}$  [40]. There are three strong absorption lines in the wavelength range 1531.5–1531.75 nm, whose simulated absorbances are plotted in Fig. 1. Two of three lines overlap with two weak neighboring absorption lines of carbon dioxide ( $\text{CO}_2$ ). Since the content of  $\text{CO}_2$  exhaled from the alveoli of a healthy individual is  $\sim 4\%$ , far higher than the exhaled level of ammonia, concentration levels of 4% and 200 ppb, at a pressure of 100 Torr, were used for  $\text{CO}_2$  (dash-dotted line) and  $\text{NH}_3$  (solid line), respectively, in the generated spectra shown in Fig. 1. Operating at low pressure is helpful in reducing the pressure broadening effect and avoiding spectral overlaps between the absorption lines. The interference-free ammonia line at 1531.68 nm ( $\bar{\nu} = 6528.77 \text{ cm}^{-1}$ ) with an absorption line strength of  $1.174 \times 10^{-21} \text{ cm}^2/\text{molecule}$  was selected as target line.

## 3. Design of custom QTF for EDFA

To realize the photoacoustic sensor system, an EDFA was employed, offering an adjustable output power from 20 mW to 3 W without variation of the laser wavelength. Being the QEPAS signal proportional to the selected absorption line strength, in terms of detection sensitivity, the watt-level amplified output power of the EDFA can effectively compensate the  $\text{NH}_3$  low absorption line strengths falling in the near-IR spectral region, which are about two orders of magnitude weaker than the corresponding lines falling in the mid-IR range. Moreover, the commercial availability of mid-IR semiconductor laser sources, such as

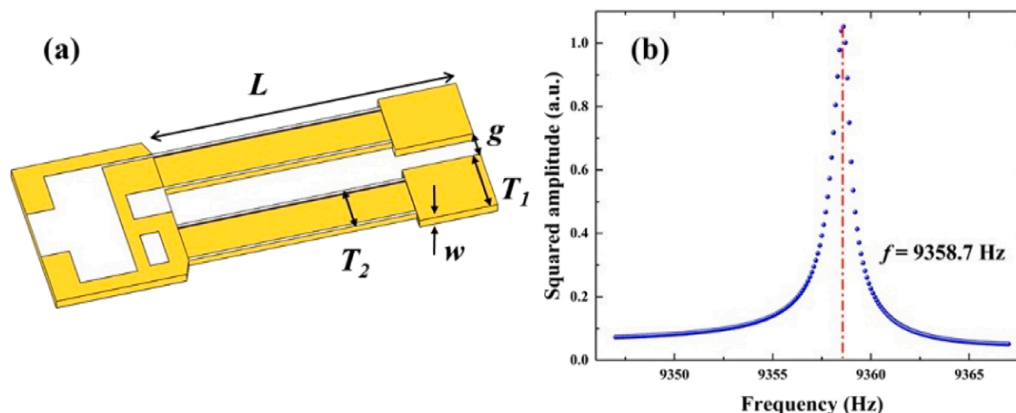


Fig. 2. (a) Schematic diagram of the T-shaped QTF. (b) Frequency response curve of the T-shaped grooved QTF at atmospheric pressure.

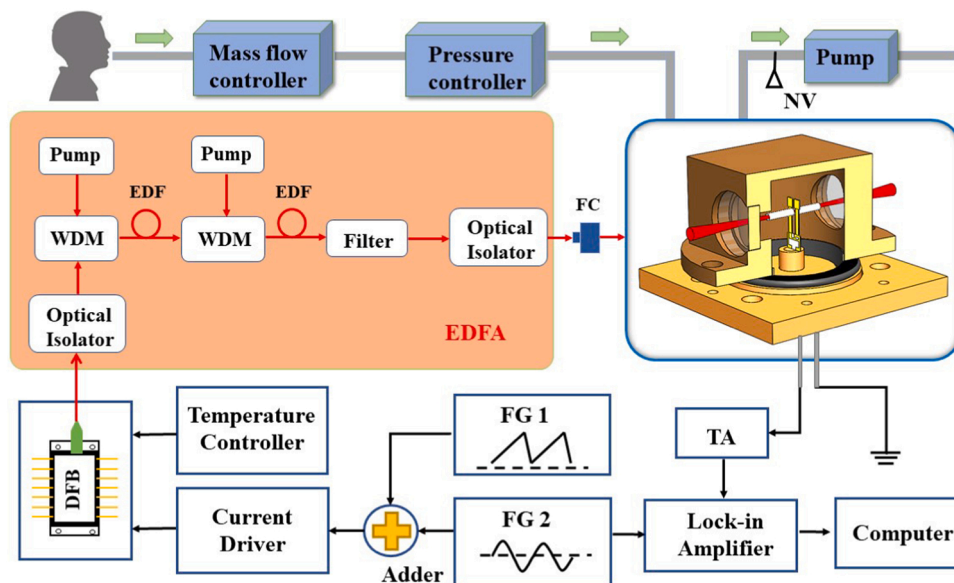


Fig. 3. Schematic of the QEPAS-based sensor system for exhaled ammonia detection. EDFA: Erbium-doped fiber amplifier; NV: needle valve; FG: Function Generator; TA: Transimpedance Amplifier; WDM: Wavelength Division Multiplexing.

quantum cascade lasers, has a high cost and heat dissipation issue, the combination of a small sized and low-cost near-infrared DFB lasers with an EDFA is an alternative technology. The design of the custom QTF for the EDFA needs to consider three aspects: (1) large prong spacing to match the high-power laser beam exiting the EDFA; (2) a high Q factor to achieve a high sensitivity; (3) a low resistance to enhance the piezoelectric conversion efficiency of the QTF.

Based on the laser beam quality of the EDFA, a prong spacing of 1 mm is large enough to effectively reduce the background noise generated by tail of the optical beam hitting the QTF [18]. A hammer-like structure was designed on the QTF tine, increasing the top weight of the QTF and thus increase the generated prongs stress field. An increase of the amplitude of the stress field produces an increase of the piezoelectrically induced charges, and subsequently an enhancement of the QTF current signal. The reported QTF is referred as T-shaped grooved QTF, whose schematic and geometrical parameters are shown in Fig. 2(a). The prong length  $L$ , thickness  $w$ , and prong spacing  $g$  of the

T-shaped grooved QTF are 9.4 mm, 2 mm, and 1 mm, respectively. The width of the hammer-shaped part  $T_1$  and non-hammer-shaped part  $T_2$  of the QTF prongs are 2 mm and 1.4 mm, respectively. In addition, four 50- $\mu\text{m}$  deep rectangular grooves was carved on the surface of each QTF prong, decreasing the distance between two electrodes and leading to a low QTF resistance, thereby increasing the generated signal [18]. The response curve of the T-shaped grooved QTF is shown in Fig. 2(b). At a pressure of 100 Torr, the resonant frequency, quality factor, and equivalent resistance of the QTF are 9358.7 Hz, 15,866, and 139.2 k $\Omega$ , respectively.

#### 4. Photoacoustic sensor system

The schematic diagram of the EDFA-based QEPAS sensor for exhaled ammonia detection is depicted in Fig. 3. A near-infrared distributed feedback (DFB) diode laser (NTT Electronics Corporation model NLK1C5J1AA) with a center emission wavelength of 1531.68 nm served

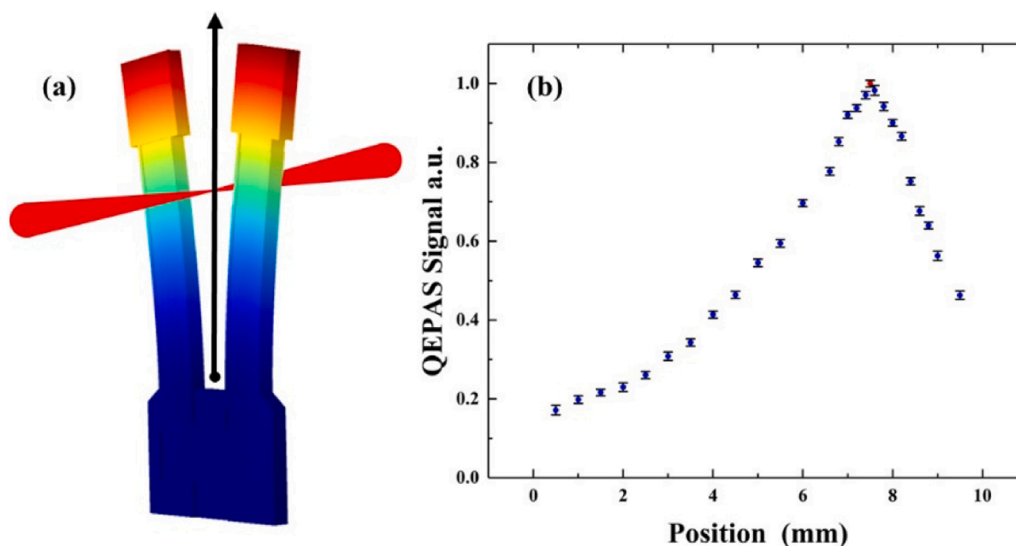


Fig. 4. (a) Sketch of a QTF depicting the prong deformation when the laser is focused on the QTF symmetry axis (Black arrow). (b) Normalized QEPAS signals obtained at different laser focal point locations. The positions on the x-axis are measured starting from the prongs bottom.

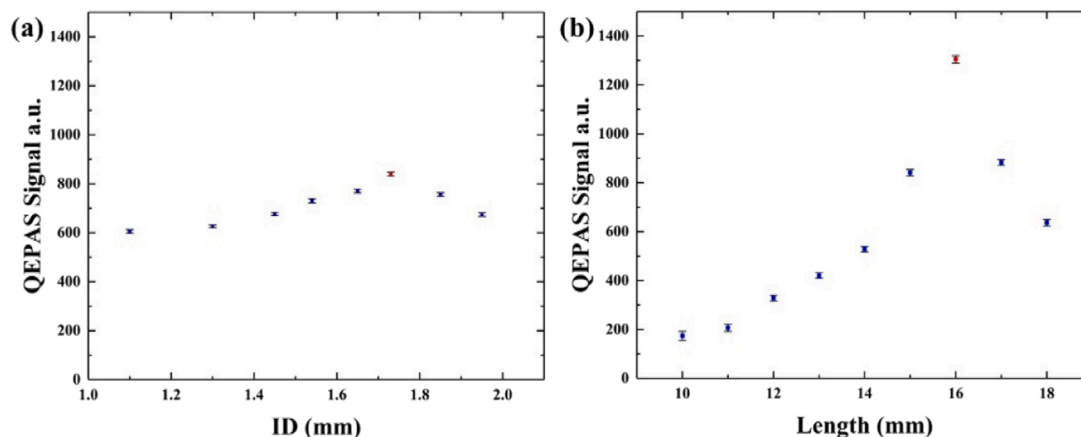


Fig. 5. (a) The relationship between the normalized QEPAS signal and the ID of the AmRs, ID: inner diameter of the tube. (b) The normalized QEPAS signal as a function of tube length.

as the excitation source. The temperature controller and current driver are integrated on the drive board to control the output wavelength of the laser. The 30 MHz ramp signal generated from a function generator slowly scans the laser wavelength across the absorption line of interest. In addition, the current of the laser was sinusoidally modulated at  $f_0/2$ , where  $f_0$  was the resonance frequency of the custom QTF. The laser beam with an output power of 20 mW was directed to the C-band EDFA (BKtel THPOA-SP400ac-FCAPC) with a two-stage amplifier, which has an output power stability of < 2%. Two optical isolators were utilized at the entrance and exit of the EDFA to protect the DFB diode laser against back reflections. The outgoing laser beam was collimated by a fiber-coupled collimator (FC) with a transmittance of 95% at  $\sim 1.5 \mu\text{m}$ , resulting in a collimating laser beam with a diameter of 650  $\mu\text{m}$ , which allowed the laser beam to easily pass through the QTF prongs without hitting their surfaces.

The excited photoacoustic signal was detected by the custom QTF and amplified by a low noise trans-impedance amplifier with a 10-M $\Omega$  feedback resistor. Then the amplified signal was demodulated by the lock-in amplifier (Stanford Research Systems, model SR830) in the  $2f$  mode with regards to the synchronous reference signal provided by the function generator (FG2). The time constant and slope filter of this lock-in amplifier were 300 ms and 12 dB/oct, respectively, resulting in a detection bandwidth of 0.833 Hz. The gas pressure in the 70  $\text{cm}^3$  gas cell was controlled at 100 Torr by a compact pressure controller (MKS Instrument Inc., U.S.A., Model 649B) in all measurements. The flow of human exhaled gas was set to a constant value of 80 sccm, which is the available maximum flow rate due to the low pressure. A flowmeter

(Alicat Scientific, Inc. Model M-500SCCMD) was used to monitor the gas flow rate simultaneously.

As shown in Fig. 4(a), the optimal sound excitation position for the QTF were determined by comparing the QEPAS signals generated by the laser beam focusing at different positions along the QTF symmetry axis. The experimental QEPAS signals, normalized to the maximum value and measured as a function of the laser focus positions, are shown in Fig. 4 (b). The optimal laser focus position was determined to be 7.5 mm away from the bottom of the QTF prongs.

Significant enhancements of the QEPAS signal-to-noise ratio have been obtained by implementing acoustic micro-resonators (AmRs) in on-beam QEPAS. For this configuration an AmR typically consists of two stainless steel tubes with the QTF positioned perpendicularly between them to probe the acoustic vibration excited in the gas contained inside the tubes [18]. The distance between the QTF and the tubes was set at 100  $\mu\text{m}$  and the geometric parameters of the AmR were optimized. The normalized QEPAS signal vs the AmRs inner diameter (ID) is shown in Fig. 5(a). The optimum ID of the AmRs was determined to be 1.7 mm. Since the cross-sectional dimensions of the optimum AmR are much smaller than the acoustic wavelength ( $\lambda_s \cong 37.8 \text{ mm}$  for  $f_0 \cong 9 \text{ kHz}$ ), a standing wave propagating longitudinally along the resonator was just excited, generating a one-dimensional acoustic field.

By optimizing the length of the single tube, the first-order longitudinal mode of the acoustic wave can match the resonance frequency of the QTF. According to the theory published in Ref [25], the optimum length of each tube is between  $\lambda_s/2$  and  $\lambda_s/4$ , where  $\lambda_s$  is the sound wavelength. As shown in Fig. 5(b), the normalized QEPAS signal rises at

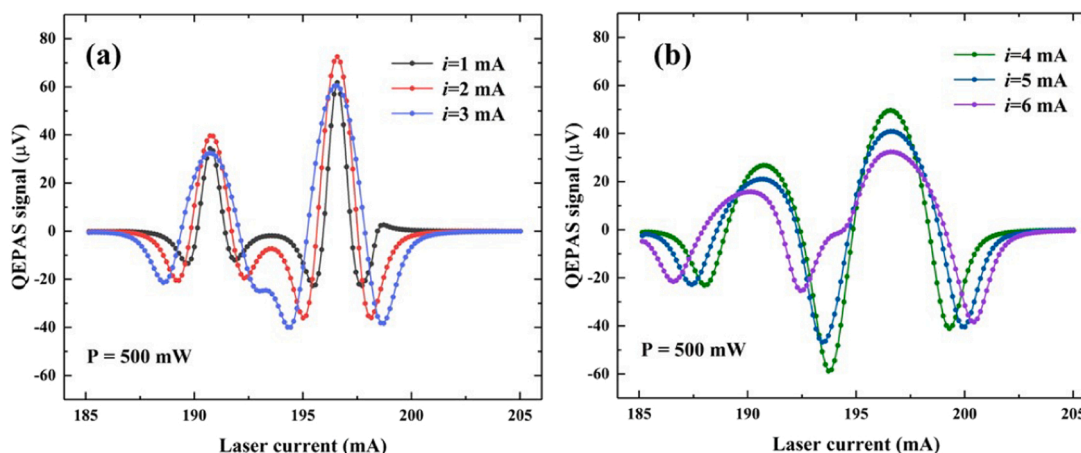


Fig. 6. The  $2f$  signal measured at different modulation currents from 1 mA to 3 mA (a) and 4–6 mA (b).



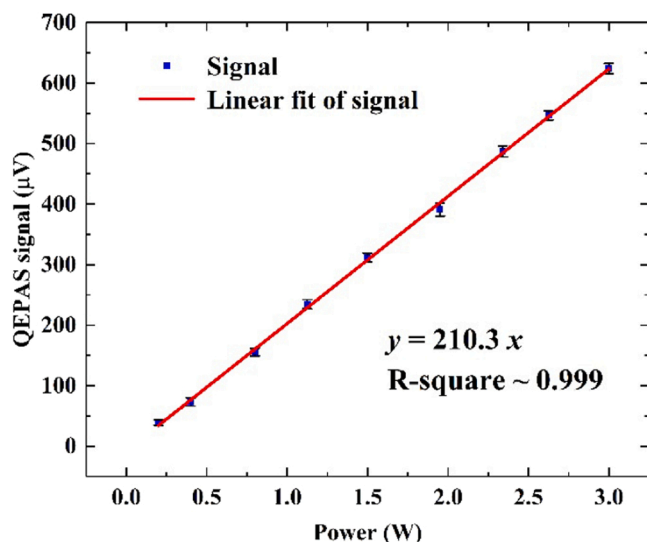


Fig. 7. QEPAS signals peak value as a function of actual excitation power.

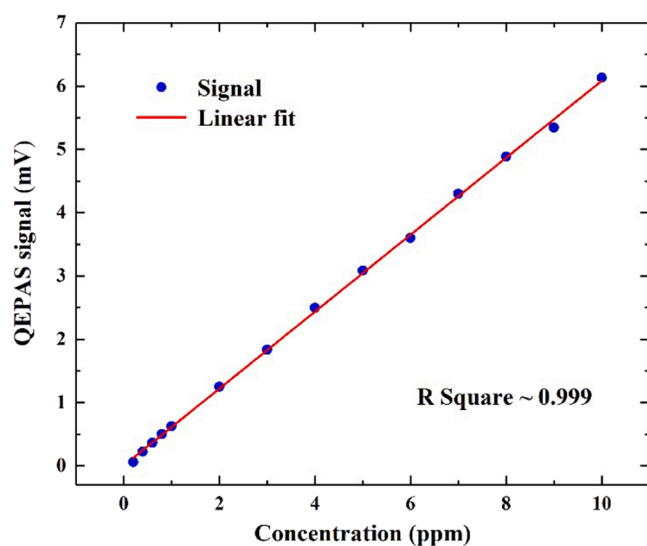


Fig. 8. Amplitudes of the 2f signal as a function of the NH<sub>3</sub> concentrations from 0.2 ppm to 10 ppm in air.

increasing the tube length, and then reaches the maximum value at  $l = 16$  mm, where the strongest acoustic coupling between the QTF and the AmRs is obtained.

### 5. Optimization of experimental parameters

For the QEPAS-based sensor, the signal amplitude is dependent on the laser current modulation depth. Thus, the modulation depth was optimized experimentally to obtain the highest QEPAS signal. A 1 ppm NH<sub>3</sub>/air mixture was fed into the chamber as a gas sample and the QEPAS signal was measured at different modulation depths from 1 mA to 6 mA when the laser wavelength slowly sweeps across the target NH<sub>3</sub> absorption line ( $\bar{\nu} = 6528.77$  cm<sup>-1</sup> for  $I = 196$  mA), for an optical emitted power of 500 mW. As shown in Fig. 6, the maximum QEPAS signal was achieved at the modulation current of 2 mA. At larger modulation current the QEPAS signals of the two NH<sub>3</sub> absorption lines at 6528.77 cm<sup>-1</sup> and 6528.91 cm<sup>-1</sup> begin to merge. Therefore, an optimal modulation depth of 2 mA was adopted in the following investigations.

The detection sensitivity of the QEPAS-based sensor is proportional to the excitation laser power. However, with laser power increasing,

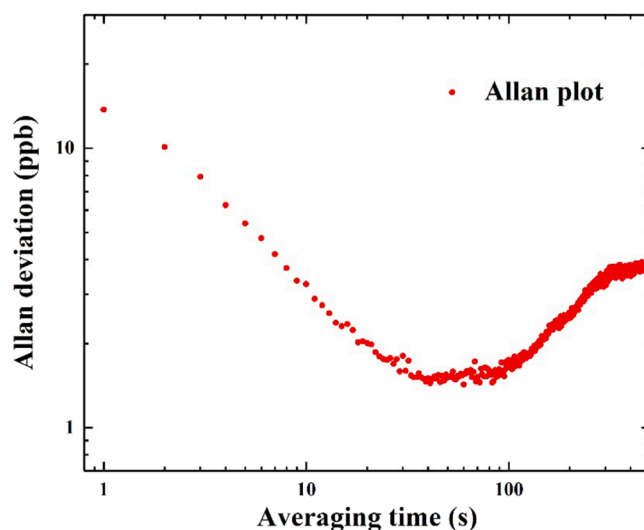


Fig. 9. Allan-Werle deviations as a function of the averaging time for pure air gas samples.

saturation effects may occur, which means that the depletion from the vibrational excited level slows with respect to the pump rate, and thus molecules are unable to be excited to higher energy levels. Thereby, we measured the QEPAS signal vs optical power in the range 200 mW–3 W for 1 ppm NH<sub>3</sub>/air mixture, to verify our sensor system was not operated in saturation. The obtained results are shown in Fig. 7.

The signal amplitude increases linearly with the increase of actual excitation power, while the sensor noise was constantly kept at  $\mu$ V level thanks to the large prongs gap of the custom QTF, proving that the sensor is not operated in saturation condition.

### 6. Results and discussion

To evaluate the performance of the sensor system for NH<sub>3</sub> detection, the system was operated at the optimized values of modulation depth and the excitation power of 3 W. The peak values of the 2f signal have been measured at different NH<sub>3</sub> concentrations, starting from a certified concentration of 10 ppm NH<sub>3</sub>:standard air and diluting down to 0.2 ppm in air using a gas mixer with 1.5% of water added and the obtained results are plotted in Fig. 8. Each data point in the figure represents the average of 50 repeated measurements. An  $R$ -square value of 0.999 was obtained through a linear fit, which confirmed that the sensor system linearly responds to the NH<sub>3</sub> concentration. The sensor noise was defined as the  $1\sigma$  standard deviation (2.13  $\mu$ V) of the signal when the pure air was introduced in the gas cell. With 200-ppb NH<sub>3</sub>/air mixture flushed into the system, a minimum detection limit (MDL) of 14 ppb was measured in a detection bandwidth of 0.833 Hz. A normalized noise equivalent absorption (NNEA) value of  $8.15 \times 10^{-9}$  cm<sup>-1</sup> W/ $\sqrt{\text{Hz}}$  was achieved.

An Allan-Werle deviations analysis was performed to evaluate the long-term stability of the NH<sub>3</sub> sensor. The gas chamber was filled with air, at a pressure of 100 torr, and the output wavelength of the laser was locked to the NH<sub>3</sub> absorption line at 6528.77 cm<sup>-1</sup>. The Allan deviation result plotted in Fig. 9 shows that the detection limit of the NH<sub>3</sub> sensor can be improved if increasing the averaging time. For an averaging time up to 40 s, the Allan-Werle deviation plots follows a  $1/\sqrt{t}$  dependence, which means that the white noise of the sensor is the dominant noise source. At an averaging time of 40 s an NH<sub>3</sub> MDL of 1.5 ppb has been achieved.

These performances pave the way to the application of the developed sensor system for environmental and biomedical applications. As proof of this last statement, the NH<sub>3</sub> sensor system was successfully tested for online detection of human exhaled ammonia. The exhaled breath from

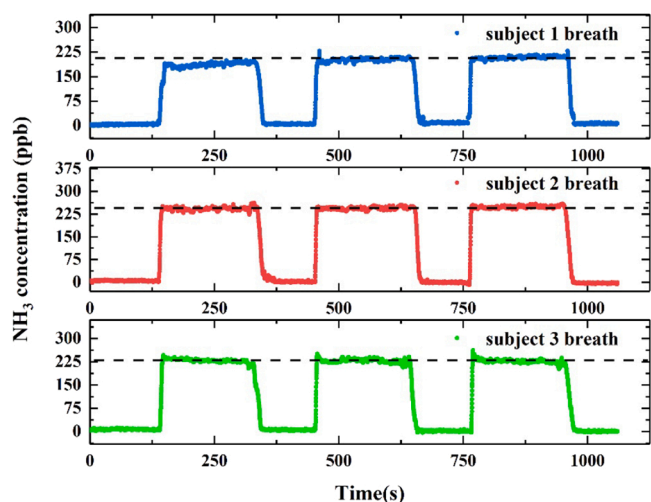


Fig. 10. Online concentration measurements of exhaled ammonia by three healthy subjects.

three volunteers was introduced into the gas chamber in real time by a custom exhaled gas sampling apparatus, a Nafion humidifier was inserted inline to keep the water concentration entering the QEPAS cell at 1.5% to eliminate the influence of environmental water vapor changes on the experimental system. A pump located downstream of the gas path was continuously operated to ensure the flow rate and pressure of the gas in the chamber. Fig. 10 shows the measurement results of the exhaled ammonia by 3 healthy subjects. Two minutes after the timer started, the exhaled ammonia gas was collected by the gas sampling apparatus and transmitted to the detection module. The measurement process lasted three minutes for online monitoring of ammonia levels exhaled by the subjects over a long period of time, rather than the changes in the ammonia concentration of the subjects exhaled in one breath.

When the exhaled breath was no longer fluxed into the detection module, the QEPAS decreases rapidly to the noise level, demonstrating that no-memory effects are present. The measurement process of exhaled ammonia by three healthy subjects was repeated three times to verify the stability of the  $\text{NH}_3$  sensing system. A signal rise/fall time of  $\sim 15$  s was achieved and exhaled ammonia levels in the range 170–230 ppb was observed. The small bumps at the beginning of each detection window in the measurements of the breath of subject 3 reflects the ammonia concentration in the oral cavity. This higher concentration is mostly related to oral bacterial processes of ingested food and beverages [41]. The signal dither observed was caused by instability in respiratory rate.

## 7. Conclusions

An  $\text{NH}_3$  QEPAS sensor implementing an erbium-doped fiber amplifier and a custom T-shaped grooved QTF with prong spacing of 1 mm was demonstrated. Our previous experimental results show that there is a significant background noise from an 800- $\mu\text{m}$ -prong-spacing QTF when the laser power is amplified to watt-levels. Therefore, a novel QTF with a prongs gap of 1 mm was designed here. The wider prongs gap of the custom QTF significantly reduces the photoacoustic noise caused by the stray light hitting the prongs of QTF. Due to the increase in excitation power, a lower MDL of 14 ppb at 1 s averaging time, corresponding to a NNEA of  $8.15 \times 10^{-9} \text{ cm}^{-1} \text{ W}/\sqrt{\text{Hz}}$ , has been achieved. The MDL reduces to 1.5 ppb if increasing the averaging time to 40 s. The obtained performances allow the implementation of the  $\text{NH}_3$  QEPAS sensor for  $\text{NH}_3$  monitoring in exhaled human breath. The experimental results confirm the potentiality of the developed  $\text{NH}_3$  sensor to be implemented for renal disease screening and monitoring of treatment progress of

patients with end-stage renal pathology, whose exhaled ammonia level is usually  $> 1$  ppm.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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